A new approach to parameterize ice-phase cloud microphysics The Predicted Particle Properties (P3) Scheme

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Development of Bulk Microphysics schemes

- Kessler (1969), first bulk scheme (liquid only, 1-moment)
- Ice-phase categories were introduced; over the next decades more detailed 1-moment schemes were developed
- In the early 2000s, 2-moment schemes (and one 3-moment scheme) appeared
- In the last 10 years, new schemes have been developed (and older ones have been improved)
 - e.g. WRF (community model) now has several schemes (12+)
 - in universities, research labs, etc. several innovative parameterization ideas have been (and are being) explored

From RPN Seminar Series March 1, 2013:

Paradigm shift (in the parameterization of ice phase) Currently under development*:

KA-ice



- ICE-PHASE HYDROMETEOR (1 mode)
- ρ is predicted
- $V = a(\rho)D^{b(\rho)}$
- Predicted rime fraction
- Predicted spectral dispersion

PROGNOSIC VARIABLES: Q_{dep}, Q_{rim}, N, B, Z

*collaboration between NCAR and RPN

OUTLINE

- 1. Background
- 2. Overview of the P3 scheme
- 3. Model results
- 4. The future ...

Vonnegut's Challenge:*

"Any scientist who can't explain to an eight-year old what he is doing is a charlatan."



* Kurt Vonnegut Jr., "Cat's Cradle", 1963

1. Background

Role of Clouds in NATURE

- radiative forcing
- thermodynamical feedback
- redistribution of atmospheric moisture
- precipitation
- etc.



Representation of Clouds in MODELS

1. Radiative Transfer Scheme

computes radiative fluxes SW/LW

2. Microphysics Parameterization Scheme

- optical properties (for radiation scheme)
- feedback to dynamics
 - latent heating/cooling
 - mass loading
- precipitation

3.Subgrid-scale schemes

• e.g. shallow convection



Microphysics Parameterization Scheme

To achieve its roles, it must represent a complex set of processes



BAMS, 1967

Microphysics Parameterization Scheme

Hydrometeors are partitioned into categories



Microphysics Parameterization Scheme

The particle size distributions are modeled



For each category, microphysical processes (initiation, growth/decay, sedimentation) are parameterized in order to predict the evolution of the <u>particle size distribution, N(D)</u>

TYPES of SCHEMES:



Liquid Phase

"Warm rain" coalescence process:

ightarrow 2-moment bulk schemes model this process very well



Ice Phase

Traditional bulk approach:



CLOUD ICE $\rho_s = 500 \text{ kg m}^{-3}$ $m = (\pi/6 \rho_s)D^3$ $V = a_i D^{b_i}$ "SNOW" $\rho_s = 100 \text{ kg m}^{-3}$ $m = cD^2$ $V = a_s D^{bs}$



GRAUPEL $\rho_g = 400 \text{ kg m}^{-3}$ $m = (\pi/6 \rho_g)D^3$ $V = a_a D^{bg}$



HAIL $\rho_h = 900 \text{ kg m}^{-3}$ $m = (\pi/6 \rho_h)D^3$ $V = a_h D^{bh}$

← abrupt / unphysical conversions

Problems with pre-defined categories:

- **1. Real ice particles have complex shapes**
- 2. Conversion between categories is ad-hoc
- 3. Conversion leads to large, discrete changes in particle properties

NOTE: Bin microphysics schemes have the identical problem



The simulation of ice-containing cloud systems is often *very sensitive* to how ice is partitioned among categories



Ice Phase

TRADITIONAL:



Partial mitigation to the problems with pre-defined categories

* Milbrandt and Morrison (2013), JAS

Which of the following is more duck-like?



- has a label that says "DUCK"
- big, round eyes
- plastic exterior, hollow interior
- yellow, wing-like appendages
- no feet
- makes a "squeak" noise



- has no label
- small, round eyes
- feathery exterior, meaty interior
- white, wing-like appendages
- webbed feet
- makes a "quack" noise

IF IT QUACKS LIKE A DUCK

2. Overview of P3

New Bulk Microphysics Parameterization: Predicted Particle Properties (P3) Scheme*

Based on a conceptually different approach to parameterize ice-phase microphysics.

NEW CONCEPT

"free" category – predicted properties, thus freely evolving type "fixed" category – traditional; prescribed properties, predetermined type

Compared to traditional (ice-phase) schemes, P3:

- avoids some necessary evils (category conversion, fixed properties)
- has self-consistent physics
- is better linked to observations
- is more computationally efficient

* Morrison and Milbrandt (2014) [P3, part 1] *J. Atmos. Sci.* (in press)

Prognostic Variables: (advected)

LIQUID PHASE:	2 categories, 2-moment:	
	Q_c – cloud mass mixing ratio	[kg kg⁻¹]
	Q_r – rain mass mixing ratio	
	N_c – cloud number mixing ratio	[#kg⁻¹]
	N_r – rain number mixing ratio	[#kg⁻¹]

nCat categories, 4 prognostic variables each:			
$p(n)^*$ – deposition ice mass mixing ratio	[kg kg⁻¹]		
Q _{rim} (n) – rime ice mass mixing ratio [kg kg ⁻¹			
$N_{tot}(n)$ – total ice number mixing ratio [#			
rim(n) – rime ice volume mixing ratio [m ³ kg ⁻			
e e t	$a_{p}(n)^*$ – deposition ice mass mixing ratio $a_{p}(n)^*$ – deposition ice mass mixing ratio $a_{n}(n)$ – rime ice mass mixing ratio $a_{t}(n)$ – total ice number mixing ratio $a_{n}(n)$ – rime ice volume mixing ratio		

* $Q_{tot} = Q_{dep} + Q_{rim}$, total ice mass mixing ratio (actual advected variable)

A given (free) category can represent any type of ice-phase hydrometeor

Prognostic Variables:	
$\boldsymbol{Q_{dep}}$ – deposition ice mass mixing ratio	[kg kg⁻¹]
Q _{rim} – rime ice mass mixing ratio	[kg kg ⁻¹]
N _{tot} – total ice number mixing ratio	[# kg ⁻¹]
B _{rim} – rime ice volume mixing ratio	[m ³ kg ⁻¹]
Predicted Properties:	
F_{rim} – rime mass fraction, $F_{rim} = Q_{rim} / (Q_{dep} + Q_{rim})$	[]
$ ho_{rim}$ – rime density, $ ho_{rim}$ = Q_{rim} / B_{rim}	[kg m ⁻³]
$m{D}_{m}$ – mean-mass diameter, $D_{m} \propto (Q_{dep} + Q_{rim}) / N_{tot}$	[m]
V_m – mass-weighted fall speed, $V_m = f(D_m, \rho_{rim}, F_{rim})$	[m s ⁻¹]
etc.	

Diagnostic Particle Types:

Based on the predicted properties (rather than pre-defined)



Overview of P3 Scheme

GENERAL (all schemes)



Overview of P3 Scheme

GENERAL (all schemes)



GENERAL (all schemes)

$$Q^{+} = Q^{0} + \Delta Q \Big|_{PROC_{-1}} + \Delta Q \Big|_{PROC_{-2}} + \dots$$

$$\Delta Q \Big|_{PROC_{-1}} = \Delta t \cdot \frac{1}{\rho} \int_{0}^{\infty} \frac{dm(D)}{dt} \Big|_{PROC_{-1}} N(D) dD$$

 $\propto M^{(p)}$ (and other moments)

Computing the tendencies for the prognostic variables (i.e. process rates) essentially amounts to computing various moments of N(D)

Predicting process rates for $V_x \rightarrow computing various M_x^{(p)}$

$$M^{(p)} = \int_0^\infty D^p N(D) dD = \int_0^\infty D^{p+\mu} e^{-\lambda D} dD$$

$$N_x(D) = N_{0x} D^{\mu_x} e^{-\lambda_x D}$$

V = prognostic variable (Q, N, ...) x = category (rain, ice, ...)

TRADITIONAL SCHEMES (e.g. 2-moment)

$$M^{(p)} \equiv \int_0^\infty D^p N_x(D) dD = N_{0x} \frac{\Gamma(1+\mu_x+p)}{\lambda_x^{p+1+\mu_x}}$$

Fixed categories, therefore *m*-*D* parameters* are constants

$$Q = \frac{1}{\rho} \int_0^\infty m(D) N(D) dD = \frac{1}{\rho} \int_0^\infty \alpha D^\beta N_x(D) dD = \frac{\alpha}{\rho} M^{(\beta)} = \frac{\alpha}{\rho} N_{0x} \frac{\Gamma(1 + \mu_x + \beta)}{\lambda_x^{1 + \mu_x + \beta}}$$
$$N = \int_0^\infty N_x(D) dD = M^{(0)} = N_{0x} \frac{\Gamma(1 + \mu_x)}{\lambda_x^{1 + \mu_x}}$$

- impose assumption about μ
- 2 equations, 2 unknowns \rightarrow solve for λ , N_0
- \rightarrow Now, any $M^{(p)}$ can be computed analytically

*
$$m(D) = \alpha D^{\beta}$$

P3 SCHEME

$$M^{(p)} \equiv \int_0^\infty D^p N_x(D) dD = N_{0x} \frac{\Gamma(1 + \mu_x + p)}{\lambda_x^{p+1+\mu_x}}$$

Fixed category \Rightarrow constant *m*-*D* parameters **Free category** \Rightarrow <u>variable</u> *m*-*D* parameters

$$Q = \frac{1}{\rho} \int_0^\infty m(D) N(D) dD = \frac{1}{\rho} \int_0^\infty \alpha D^\beta N_x(D) dD = \frac{\alpha}{\rho} M^{(\beta)} = \frac{\alpha}{\rho} N_{0x} \frac{\Gamma(1 + \mu_x + \beta)}{\lambda_x^{1 + \mu_x + \beta}}$$

 \rightarrow cannot compute *Q* analytically (or any other *M*^(*p*))

P3 SCHEME – Determining $m(D) = \alpha D^{\beta}$ for regions of D:

Conceptual model of particle growth following Heymsfield (1982):



 $\begin{array}{l} \alpha = n \circ \rho_{0} \\ \beta = 3 \end{array}$

P3 SCHEME – Determining $m(D) = \alpha D^{\beta}$ for regions of *D*:



P3 SCHEME – Determining $m(D) = \alpha D^{\beta}$ for regions of D:



P3 SCHEME – Computing N(D) parameters :

- 1. Compute properties $F_{rim} = Q_{rim}/(Q_{dep}+Q_{rim})$, $\rho_{rim} = Q_{rim}/B_{rim}$
- 2. Determine integral ranges, D_{th} , D_{gr} , D_{cr}
- 3. Determine PSD parameters (λ , N_0 , μ)
 - apply definitions of Q_{tot} and N_{tot}

$$Q = \frac{1}{\rho} \left[\int_{0}^{D_{th}} \alpha_1 D^{\beta_1 + \mu} e^{-\lambda D} dD + \int_{D_{th}}^{D_{gr}} \alpha_2 D^{\beta_2 + \mu} e^{-\lambda D} dD + \int_{D_{gr}}^{D_{cr}} \alpha_3 D^{\beta_3 + \mu} e^{-\lambda D} dD + \int_{D_{cr}}^{\infty} \alpha_4 D^{\beta_4 + \mu} e^{-\lambda D} dD \right]$$
$$N = N_{0x} \frac{\Gamma(1 + \mu_x)}{\lambda_x^{1 + \mu_x}}$$
$$\mu = f(\lambda)$$

- solved numerically (iteratively; pre-computed and stored in look-up table)
- 4. Also, match A-D parameters to m-D parameters for the various regions of D
 - based on geometric + empirical relations
 - for *V-D* (process rates and sedimentation) and r_{i_eff} (optical properties)

P3 SCHEME – Computing the process rates:

Now, have λ , N_{0} , μ , and integral ranges D_{th} , D_{gr} , D_{cr} (plus $\alpha_{(i)}$, $\beta_{(i)}$, ...) **RECALL**:



P3 SCHEME – Computing the process rates:

Now, have λ , N_0 , μ , and integral ranges D_{th} , D_{gr} , D_{cr} (plus $\alpha_{(i)}$, $\beta_{(i)}$, ...)

ACTUALLY, FOR P3:

$$Q^{+} = Q^{0} + \Delta Q \Big|_{PROC_{-1}} + \Delta Q \Big|_{PROC_{-2}} + \dots$$

$$\Delta Q \Big|_{PROC_{-1}} = \Delta t \cdot \frac{1}{\rho} \int_{0}^{\infty} \frac{dm(D)}{dt} \Big|_{PROC_{-1}} N(D) dD$$

$$\propto X_{1} \quad (\text{and } X_{2}, \dots)$$

$$X_{1} = \int_{0}^{D_{th}} D^{a} N_{0} e^{-\lambda D} f(\alpha_{1}, \beta_{1}, \dots) dD + \int_{D_{th}}^{D_{sr}} D^{b} N_{0} e^{-\lambda D} f(\alpha_{2}, \beta_{2}, \dots) dD$$

$$+ \int_{D_{sr}}^{D_{cr}} D^{c} N_{0} e^{-\lambda D} f(\alpha_{3}, \beta_{3}, \dots) dD + \int_{D_{cr}}^{\infty} D^{d} N_{0} e^{-\lambda D} f(\alpha_{4}, \beta_{4}, \dots) dD$$

Predicting process rates \rightarrow computing sums (X_n) of partial moments

P3 SCHEME – Computing the process rates:

Now, have λ , N_{0} , μ , and integral ranges D_{th} , D_{gr} , D_{cr} (plus $\alpha_{(i)}$, $\beta_{(i)}$, ...)

$$X_{1} = \int_{0}^{D_{th}} D^{a} N_{0} e^{-\lambda D} f(\alpha_{1}, \beta_{1}, ...) dD + \int_{D_{th}}^{D_{gr}} D^{b} N_{0} e^{-\lambda D} f(\alpha_{2}, \beta_{2}, ...) dD + \int_{D_{gr}}^{D_{cr}} D^{c} N_{0} e^{-\lambda D} f(\alpha_{3}, \beta_{3}, ...) dD + \int_{D_{cr}}^{\infty} D^{d} N_{0} e^{-\lambda D} f(\alpha_{4}, \beta_{4}, ...) dD$$

- All process rates are proportional to one or more sums (X₁) of sub-moments
- Relevant sums of sub-moments are pre-computed (accurately) and stored in a look-up table
- At run time, values of X_1 , X_2 ,... are accessed (quickly) via look-up table \rightarrow actual computation of $\Delta Q|_{PROC x}$ is fast

3. Model Results

3D Squall Line case: (June 20, 2007 central Oklahoma)

- WRF_v3.4.1, $\Delta x = 1$ km, $\Delta z \sim 250-300$ m, 112 x 612 x 24 km domain
- initial sounding from observations
- convection initiated by *u*-convergence
- no radiation, surface fluxes





WRF Results: Base Reflectivity (1 km AGL, t = 6 h)



Morrison et al. (2014) [P3, part 2]

WRF Results: Line-averaged Reflectivity (t = 6 h)





Vertical cross section of

 $F_r \sim 0-0.1$ $\rho \sim 900$ kg m-3 $V \sim 0.3$ m s⁻¹ $D_m \sim 100$ μm → small crystals

$$F_r \sim 0$$

 $\rho \sim 50 \text{ kg m-3}$
 $V \sim 1 \text{ m s}^{-1}$
 $D_m \sim 3 \text{ mm}$
 \rightarrow aggregates

$$F_r \sim 1$$

 $\rho \sim 900 \text{ kg m}^{-3}$
 $V > 10 \text{ m s}^{-1}$
 $D_m > 5 \text{ mm}$
 \rightarrow hail



- small, round eyes
- feathery exterior, meaty interior
- white, wing-like appendages
- webbed feet
- makes a "quack" noise
- \rightarrow duck

Frontal/orographic case: IMPROVE-2, 13-14 December 2001

• WRF_v3.4.1, $\Delta x = 3$ km, 72 stretched vertical levels



Simulated lowest level **REFLECTIVITY** (00 UTC December 14)

Accumulated **PRECIPITATION** (14 UTC Dec 13 - 08 UTC Dec 14)

Morrison et al. (2014) [P3, part 2]



Timing Tests for 3D WRF Simulations

Scheme	Squall line caseOrographic case $(\Delta x = 1 \text{ km})$ $(\Delta x = 3 \text{ km})$		<pre># prognostic variables</pre>
P3	0.436 (1.043)	0.686 (1.013)	7
MY2	0.621 (1.485)	1.012 (1.495)	12
MOR-H	0.503 (1.203)	0.813 (1.200)	9
ТНО	0.477 (1.141)	0.795 (1.174)	7
WSM6	0.418 (1.000)	0.677 (1.000)	5
WDM6	0.489 (1.170)	0.777 (1.148)	8

- Average wall clock time per model time step (units of seconds.)
- Times relative to those of WSM6 are indicated parenthetically.

\rightarrow P3 is one of the fastest schemes in WRF





The NOAA HWT Spring Forecasting Experiment is a yearly experiment that investigates the use of convection-allowing model forecasts as guidance for the prediction of hazardous convective weather. A variety of model output is examined and evaluated daily, and experimental forecasts are created and verified to test the applicability of cutting-edge tools in a simulated forecasting environment. The variety of model output allows us to explore different types of guidance, including products derived from both ensembles and deterministic forecasts, and to provide focused feedback to model developers.

The 2014 Spring Forecasting Experiment will be held from May 5th through June 6th in the HWT facility at the National Weather Center in Norman. The Experiment is scheduled to run Monday through Friday from 8am to 4pm. More information about this year's Experiment can be found below in the 2014 Spring Forecasting Experiment Operations Plan (see below).

Guidance Information

- Summary of 2014 Model Guidance
- File Status: NSSL | SPC

Model Guidance Graphics

- HWT Model Comparison Page
- Objective Verification: 1-km Sim. Reflectivity [Images w/ Scores]
- Objective Verification: 1-km Sim. Reflectivity [Score Summary]
- Experimental Ensemble graphics All Members
- Experimental Ensemble Proxy Severe Forecast | Verification
- Experimental Ensemble 3h Proxy Severe Forecast | Verification

Operation Plans and Procedures

- HWT Spring Forecasting Experiment Operations Plan
- CAPS Spring Forecasting Experiment Program Plan

Evaluation Forms (internal)

- SE2014 Evaluation of Yesterday's Forecasts: SPC Desk
- SE2014 Evaluation of Yesterday's Forecasts: NSSL/Dev Desk
- SE2014 Evaluation of Convection-Allowing Ensembles
- SE2014 Evaluation of EMC Parallel CAMs
- SE2014 HAILCAST Evaluation
- SE2014 Microphysics comparisons
- SE2014 NSSE WRF UKnet comparisons

Experimental Forecasts

- 2014 Experimental Forecast Verification Severe Convection
- 2014 Hourly Probabilistic Forecasts: NSSL/Dev Desk
- Set Forecast Centerpoint
- 2014 Experimental Forecast Generation SPC Team (Restricted)
- 2014 Experimental Forecast Generation NSSL Team

http://hwt.nssl.noaa.gov/Spring_2014



2014 OU CAPS Ensemble (4-km WRF)*



22-h FCST, 1-km Reflectivity, 22 UTC 8 May, 2014

* c/o Fanyou Kong





Simulated 10.7 MICRON Brightness Temperatures

* c/o Fanyou Kong

So far – despite using only 1 ice-phase category, P3 performs remarkably well compared to detailed, established (well-tuned), traditional bulk schemes

However – with 1 category, P3 has some <u>intrinsic limitations</u>:

- it cannot represent more than one type of particle in the same point in time and space
- As a result, there is an inherent "*dilution problem*"; the properties of populations of particles of different origins get averaged upon mixing



Single-Category Version

All ice-phase hydrometeors represented by a single category, with Q_{dep} , Q_{rim} , N_{tot} , B_{rim}

Processes:

- 1. Initiation of new particles
- 2. Growth/decay processes
 - interactions with water vapor
 - interactions with liquid water
 - self-collection
- 3. Sedimentation

Multi-Category Version

Milbrandt and Morrison (2015) [P3, part 3] (in preparation)

All ice-phase hydrometeors represented by a *nCat* categories, with $Q_{dep}(n)$, $Q_{rim}(n)$, $N_{tot}(n)$, $B_{rim}(n)$ [n = 1..nCat]

Processes:

- 1. Initiation of new particles → determine destination category
- 2. Growth/decay processes
 - interactions with water vapor
 - interactions with liquid water
 - self-collection
 - collection amongst other ice categories
- 3. Sedimentation

Multi-Category Version

Initiation of new particles -> Determining destination category

OBJECTIVE: To select the destination category of new ice such that the overall *dilution is minimized*

1. Determine category *n* with minimum $D_diff = |D_n(n) - D_new|$

2. IF *D_diff < diff_Thrs* THEN

NOTE: diff_Thrs = f(nCat)

n_Dest = next empty category (if one is available)

diffThrs	D_new	<i>D_1</i> ⁰ (diff)	<i>D_2º</i> (diff)	<i>D_3º</i> (diff)	n_Dest	D_1+	D_2⁺	D_3⁺
500	10				1	10		
500	10	15 (5)			1	14.9		
500	10	600 (590)			2	600	10	
500	10	600 (590)	400 (390)		2	600	46.6	
300	10	600 (590)	400 (390)		3	600	400	10
300	700	600 (100)	400 (200)		1	600.7	400	
300	10	600 (590)	400 (390)	350 (340)	3	600	400	46.5
300	700	500 (100)	400 (300)	350 (350)	1	501.1	400	350

All sizes in μ m

P3 – Effects of multiple categories:

1D Kinematic Model*

- user-specified number of vertical levels
- reads in a sounding to initialize T(p) and $T_d(p)$; interpolates/converts to T(z) and $q_v(z)$
- during integration:
 - time-varying updraft profile (and corresponding divergence)
 - advection of T, q_v , and all hydrometeor tracers
 - call to microphysics scheme
 - output: profiles of prognostic and diagnostic variables



* described in Milbrandt et al. (2012) **P3 – Effects of multiple categories:**

For the next few slides ...

Time-height plots of output from 1D model









 ho_{ice}







 $w_{max} = 10 \text{ m s}^{-1}$ nCat = 1



 $w_{max} = 10 \text{ m s}^{-1}$ nCat = 2



 $w_{max} = 10 \text{ m s}^{-1}$ nCat = 3

 $W_{max} = 10 \text{ m s}^{-1}$



 $W_{max} = 3 \text{ m s}^{-1}$





results in excessive dilution

P3 – Effects of multiple categories

Comments from 1D simulations:

- increasing the number of categories
 + reduces the "dilution" effect
 + results in earlier precipitation at the ground
- the number of categories to reach convergence increases with the amount of forcing

→ the multi-category version behaves as expected in 1D; ready to test in 3D

P3 Scheme – Interface in GEM (4.7.0)

Two main pieces of code: • create_lookup_table.F90 • mp_p3.F90

subroutine create_lookup_table

→ Creates multidimensional look-up table of pre-computed moments (used for process rates)

module mp_p3
subroutine p3_init
subroutine p3_wrapper_wrf
subroutine p3_wrapper_gem
subroutine p3_main

- → Reads in look-up table; computes various quantities (called on first time step only)
- \rightarrow Main interface for WRF
- → Main interface for GEM (called by CONDENSATION)
- \rightarrow Main s/r (called by wrapper)

P3 Scheme – Interface in GEM (4.7.0)

subroutine p3_main(Qitot, Qirim, Nitot, Birim, ncat, ...

real, dimension(ni, nk, ncat) :: Qitot, Qirim, Nitot, Birim

```
in s/r condensation:
```

```
IF (stcond .eq. 'mp_p3') THEN
```

etc. ...

&physics_cfgs

stcond = mp_p3 p3_ncat = 2

P3_MAIN is generalized (nCat categories)

P3_WRAPPER_GEM constructs / deconstructs array of (ni, nk, nCat) from nCat arrays (ni, nk) for each variable

ENDIF

GEM simulation with P3 (*nCat* = 1) on HRDPS (pan-Canadian) domain



12-h FCST (valid 00 UTC 9 June 2011)

GEM (2.5 km)

Reflectivity (1 km AGL)



12-h FCST (valid 00 UTC 9 June 2011)

GEM (2.5 km), P3

Reflectivity





GEM (2.5 km), P3

Precipitation Rate



Convergence with *nCat* = 2?

4. The Future...

Further Development of P3

- 1. Tuning in operational context
- 2. Additional predicted properties
 - Liquid fraction
 - Spectral dispersion (triple-moment)
 - others...
- 3. Subgrid-scale cloud fraction

P3 in GEM

- 1. Implementation into GEM_4.7.0
- 2. Consideration for HRDPS
 - P3 (*nCat* = 1) vs. P3 (*nCat* = 2)
 - P3 vs. MY2_new

Everything has a shelf-life.



EXTRA

Timings from 3D GEM runs:

- full pan-Canadian HRDPS grid

- topology 10 x 32 x 1

Run	CP SECS	GEMDM	DYNSTEP	ADW	PHYSTEP	#tracers	
(MY2_orig) (MY2_new) (P3_1cat) (P3_2cat)	7587 6641 5925 6681	9069 7927 7058 7980	4637 3685 3258 3659	3356 2470 2091 2433	4018 3891 3430 3914	12 12 7 11	
(MY2_orig) (MY2_new) (P3_1cat) (P3_2cat)	1. 0.87 0.78 0.87	(NOTE: with 10 x 32 x 4, ratio is about 0.84)					
Extra cost of ADW for extra tracers (vs Run 1) $\frac{Run}{4}$ (3356-1656)/11 = 154 s/tracer, 154/4689 = 3.3%, 154/5062 = 3.0% extra total time (per tracer) 6 (2470-1656)/11 = 74 s/tracer, 74/4689 = 1.6%, 74/5062 = 1.4% 7 (2091-1656)/6 = 73 s/tracer, 73/4689 = 1.6%, 73/5062 = 1.4% 8 (2433-1656)/10 = 78 s/tracer, 78/4689 = 1.7%, 78/5062 = 1.5%							